

# **Coil Driven Alarm Design** Considerations

## INTRODUCTION

Normally, watch circuits, such as the ICM7220A, will drive a piezoelectric ceramic transducer at 3V pp directly, with an audio output of sufficient volume for wristwatch applications, providing the transducer is designed to have a resonant frequency of about 4 kHz when circumferentially edge mounted. There may be times, however, when greater output volume is desired, and this can be achieved by the addition of three components — a transistor, an inductor, and a resistor. (See Figure 1).

This circuit uses an NPN transistor, although certain devices require use of a PNP instead. (Figure 2). Table 1 shows the circuit which should be used with currently available Intersil devices.

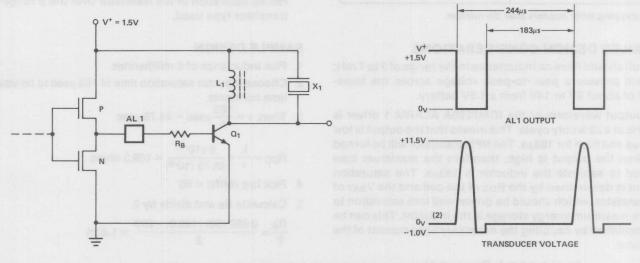


Figure 1. Use of an NPN Transistor and Associated Waveforms

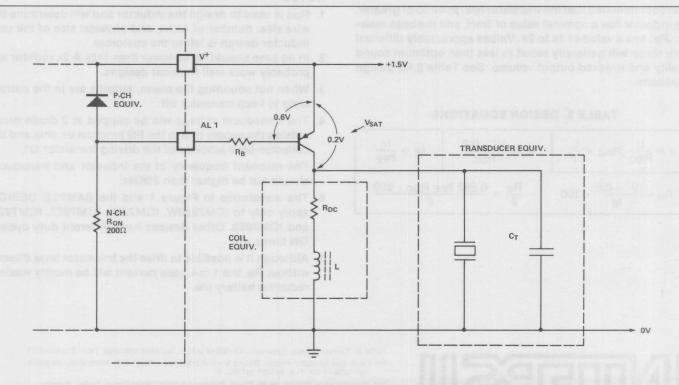


Figure 2. Equivalent Circuit Using PNP Transistor and Showing Non-Ideal Component Equivalents

## TABLE 1

Product	Die Stepping*	Circuit Figure Number
ICM7220A, MA	W	1
ICM7220FA, MFA	W	1
ICM7221	Z	2
ICM7222	Z, Y	2
ICM7222	W	1
ICM7223	all	1
ICM7052	all	2
ICM7049	all	2
ICM7050	all	2
ICM1115	all	2

\*Die stepping letter appears after die number.

# **DETAILED DESIGN CONSIDERATIONS**

The coil should have an inductance in the range of 3 to 7 mH; this will provide a peak-to-peak voltage across the transducer of about 9V to 14V from a 1.5V battery.

The output waveform of the ICM7220A ALARM 1 driver is 4096 Hz at a 25% duty cycle. This means that the output is low for  $61\mu s$  and high for  $183\mu s$ . The NPN transistor will be turned on when the output is high, therefore the maximum time allowed to saturate the inductor is  $183\mu s$ . The saturation current is determined by the Rpc of the coil and the VsAT of the transistor, which should be driven well into saturation to ensure maximum energy storage in the inductor. This can be accomplished by doubling the necessary base current of the transistor.

$$I_{B(MAX)} < 1 \text{ mA}, R_{B(MIN)} = 1k$$

It is recommended that the transistor  $h_{FE}(\beta)$  be 50 or greater, the inductor has a nominal value of 5mH, and the base resistor (R<sub>B</sub>) has a value of 1k to 2k. Values appreciably different from these will generally result in less than optimum sound quality and lowered output volume. See Table 2 for design equations.

# **TABLE 2. DESIGN EQUATIONS**

$\tau = \frac{L}{R_{DC}}$ ; $R_{DC} = \frac{L}{\tau}$	$I_C = \frac{V^+ - 0.2}{R_{DC}}$	$I_{B} \geq \frac{I_{C}}{h_{FE}}$
$R_B = \frac{V^+ - 0.6}{I_B} - 200$	$\frac{R_B}{2} = \frac{0.692 \text{ hfe RDC} - 2000}{2}$	

## **DESIGN STEPS**

When designing a coil driven alarm circuit, several things must be taken into consideration. They are:

- 1. The DC resistance of the coil (Rpc). See note 1.
- 2. The transistor B (hfe)
- 3. The L/R time constant of the inductor.
- 4. The base resistance (R<sub>B</sub>) needed to guarantee saturation of the transistor. See note 2.

The following steps should be used:

- 1. Select inductance.
- 2. Choose the time constant.
- 3. Calculate the coil resistance.
- 4. Choose a transistor with a minimum  $\beta$  (hfe).
- 5. Calculate R<sub>B</sub> and reduce calculated value by 50% to guarantee saturation of the transistor over the  $\beta$  range of the transistor type used.

### SAMPLE DESIGN

- 1. Pick inductance of 5 millihenries.
- 2. Choose inductor saturation time of 183  $\mu$ sec to be equal to 4 time constants.
- 3. Then:  $\tau = \frac{183}{4} \mu \text{sec} = 45.75 \ \mu \text{sec}$

$$R_{DC} = \frac{L}{\tau} = \frac{5 (10^{-3})}{45.75 (10^{-6})} = 109.3 \text{ ohms}$$

- 4. Pick hfE (MIN) = 50
- 5. Calculate RB and divide by 2.

$$\frac{R_B}{2} = \frac{0.692 (50) (109.3) - 200}{2} = 1.80K$$

#### NOTES:

- R<sub>DC</sub> is used to design the inductor and will determine the wire size, number of turns, and physical size of the coil. Inductor design is left to the customer.
- 2. In no case should RB be lower then 1k $\Omega$ . A 2k resistor will probably work well for most designs.
- 3. When not sounding the alarm, outputs are in the correct state to keep transistor off.
- 4. The transducer voltage will be clipped at 2 diode drops outside the supply due to the PN junction on chip and the collector-base junction of the driving transistor Q1.
- The resonant frequency of the inductor and transducer should not be higher than 20KHz.
- The waveforms in Figure 1 and the SAMPLE DESIGN apply only to ICM7220W, ICM7221, ICM7222, ICM7223, and ICM7052. Other devices have different duty cycles, ON times, etc.
- Although it is possible to drive the transistor base directly without R<sub>B</sub>, the 1 mA base current will be mostly wasted, reducing battery life.

IMIERSIL

10710 N. Tantau Avenue, Cupertino, CA 95014 U.S.A., Tel: (408) 996-5000, TWX: 910-338-0171 9th Floor, Snamprogetti House, Basing View, Basingstoke, RG21 2YS, Hampshire, England, Tel: 0256-57361, TLX: 847227 INTRSL G

217, Bureaux de la Colline, de St. Cloud, Batiment D, 92213 Saint-Cloud, Cedex, France, Tel: (1) 602-57-11, TLX: Datelem 204280F (Liaison Office)

Bavariaring 8, 8000 Munchen 2, West Germany, Tel: 89/539271, TLX: 5215736 INSL D

Intersil cannot assume responsibility for use of any circuitry described other than circuitry entirely embodied in an Intersil product. No other circuit patent licenses are implied. Intersil reserves the right to change the circuitry and specifications without notice at any time.